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WELCOME TO

PRECISE POSITIONING TECHNIQUES: GNSS ERROR SOURCES & MITIGATION



Monday, December 15, 2014

10 am–11:30 PST

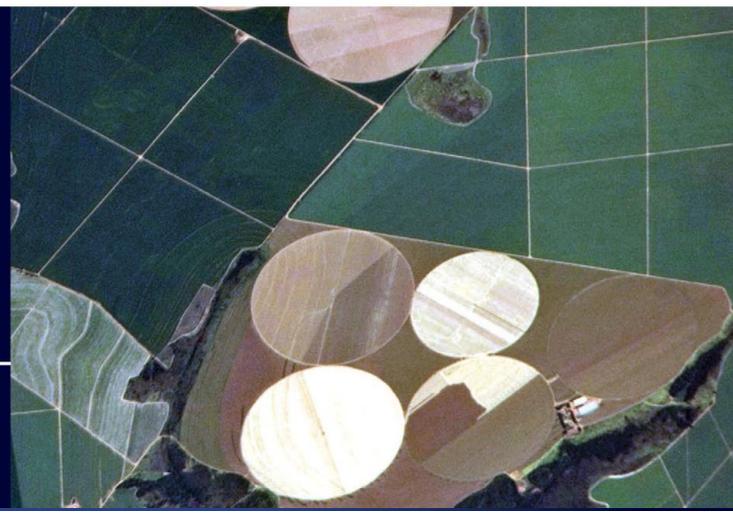
11 am–12:30 pm MST

Noon–1:30 pm CST

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WELCOME TO

Precise Positioning Techniques: GNSS Error Sources & Mitigation



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Who's In the Audience?

A diverse audience of over 900 professionals registered from 73 countries, 40 states and provinces representing the following industries:

16% GNSS Equipment Manufacturer

25% Professional User

18% System Integrator

14% Product/Application Designer

27% Other



Welcome from *Inside GNSS*



Glen Gibbons

Editor and Publisher
Inside GNSS

A word from the sponsor



Sara Masterson, P. Eng.

**New Business
Development Manager
NovAtel, Inc**

Poll #1

What level of accuracy do you currently achieve with your gnss positioning?

- *Greater than a meter*
- *Less than a meter*
- *Meter*
- *10 centimeters*
- *Less than 10 centimeters*



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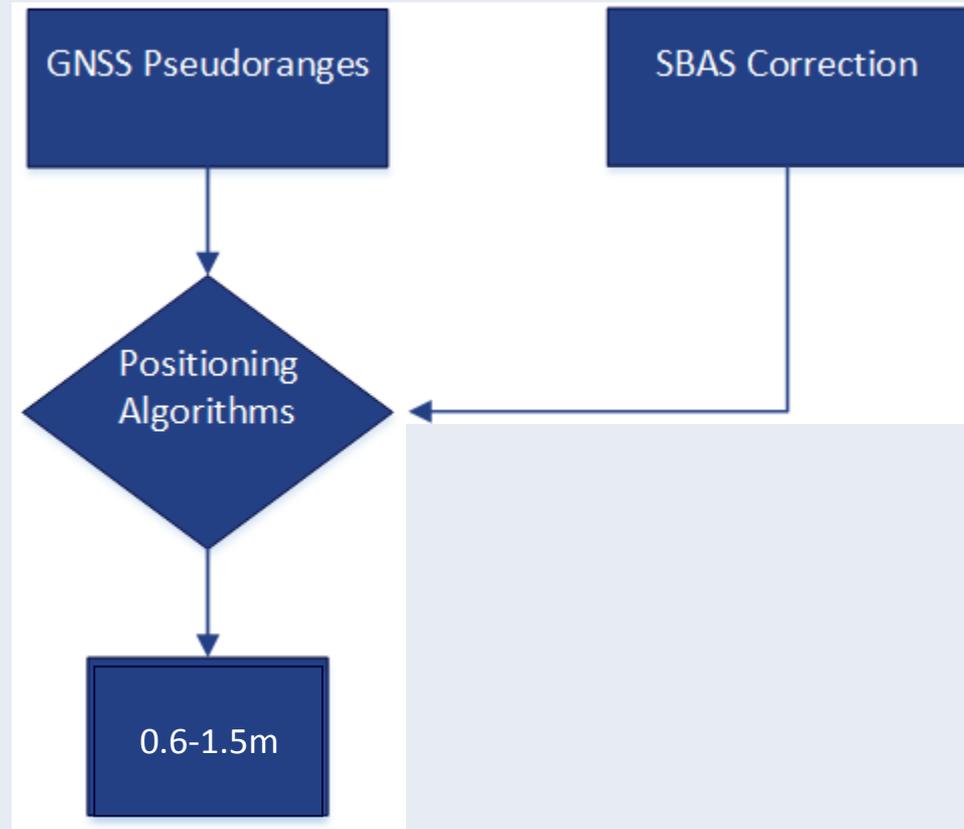


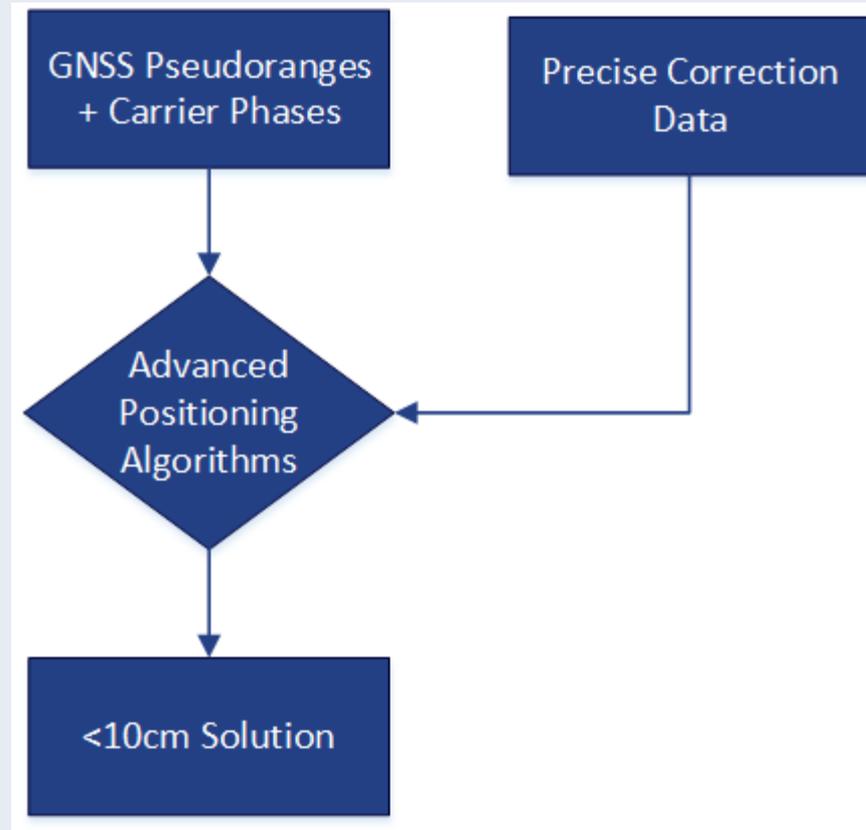
Sandy Kennedy
Director and Chief Engineer
of Core Cards
NovAtel Inc.

Precise GNSS Positioning



Sandy Kennedy
Director, Core Receiver Cards
NovAtel Inc.





- <10cm accuracy has been possible for over 10 years, why is there more interest now?
- The Enablers:
 - Easily accessible correction data
 - Advanced positioning algorithms

Correction Data

THEN

- Your own base receiver
- Radio link, limited to 3 km, affected by terrain
- Competition for radio channels
- Long delays (days) for precise orbits and clocks

NOW

- RTK correction services in most cities, broadcast over cellular frequencies
- Base station files available for post-processing (ie CORS)
- Rapid precise clocks and orbits
- Increased quality of corrections delivered over L-band/MSS

Improved Algorithms

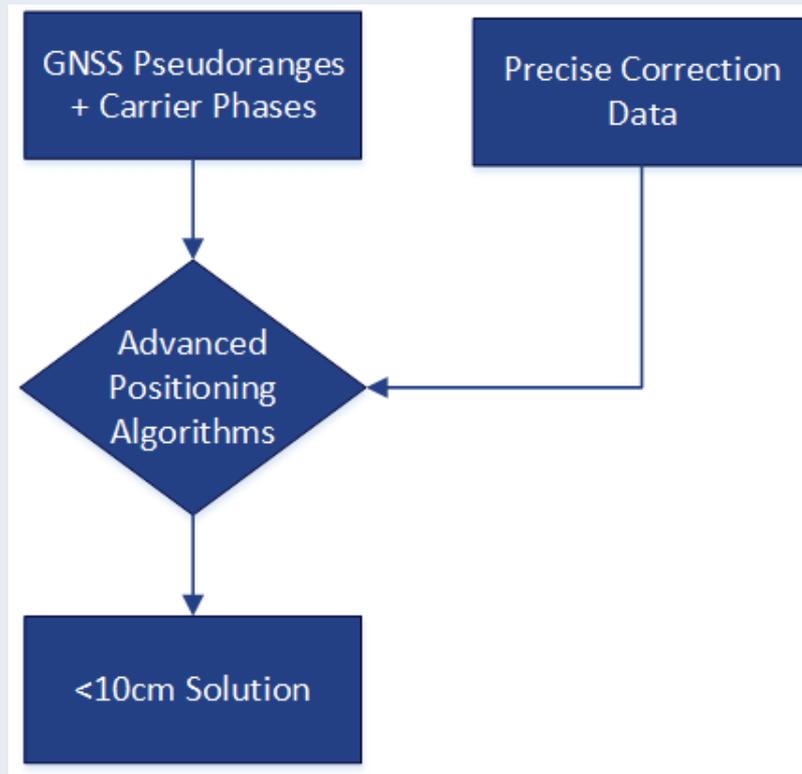
RTK

- Faster fixes over longer baselines
- Network RTK or single base station
- Reliable quality indicators

PPP

- Has come a long way!
- Popular in post-processing first, now real time
- <10cm kinematic, real-time achievable

- When your focus shifts from having a meter level position to a cm level position
 - You require good quality, precise measurements
 - Trade off decisions on antenna and receiver design may change



GNSS Antenna and Receiver Design Considerations for High Accuracy Applications

Disclaimer: The views expressed in this presentation are those of the author, and do not reflect the official policy or position of the United States Air Force, Department of Defense, or U.S. Government.



Sanjeev Gunawardena
Research Assistant Professor
Air Force Institute of Technology

- Primer on GNSS Antenna and Receiver Design
 - GPS signal link budget and S/N_0
 - GNSS antennas
 - Receiver architecture
 - Baseband signal processing

- How Range Measurements are Computed
 - Pseudorange
 - Accumulated Doppler Range
 - Carrierphase

- Considerations for High Accuracy GNSS
 - Relationship between bandwidth and measurement accuracy
 - Multipath mitigation
 - Front-end component effects
 - Signal deformation

GPS Signal

Radiated Power 14 dBW (25 W)

SV Antenna Gain (avg.) +11 dB

Free Space Loss:

$$PD = \frac{P_t}{4\pi R^2} \quad (\text{Watts/Meter}) \quad -158 \text{ dB}$$

$R \sim 22,700 \text{ km}$

Atmospheric Loss: -2 dB

Pwr. incident on $\frac{\lambda^2}{4\pi}$ -25 dB

Isotropic Antenna: $\frac{\lambda^2}{4\pi}$ +1 dB

Receive Antenna Gain +1 dB

Received Signal Power: -159 dBW

min. L1 C/A [GPS IS-200]



GPS Receiver

Thermal Noise

$$n_0(t) \sim N(0, \sigma_{n_0}^2)$$

$$\sigma_{n_0}^2 = k_B T_0 B$$

k_B : Boltzmann's constant

1.38×10^{-23} [Joules / Kelvin]

T_0 : Ambient Temperature [Kelvin]

Example: for $B=24 \text{ MHz}$, and $T=295\text{K}$:

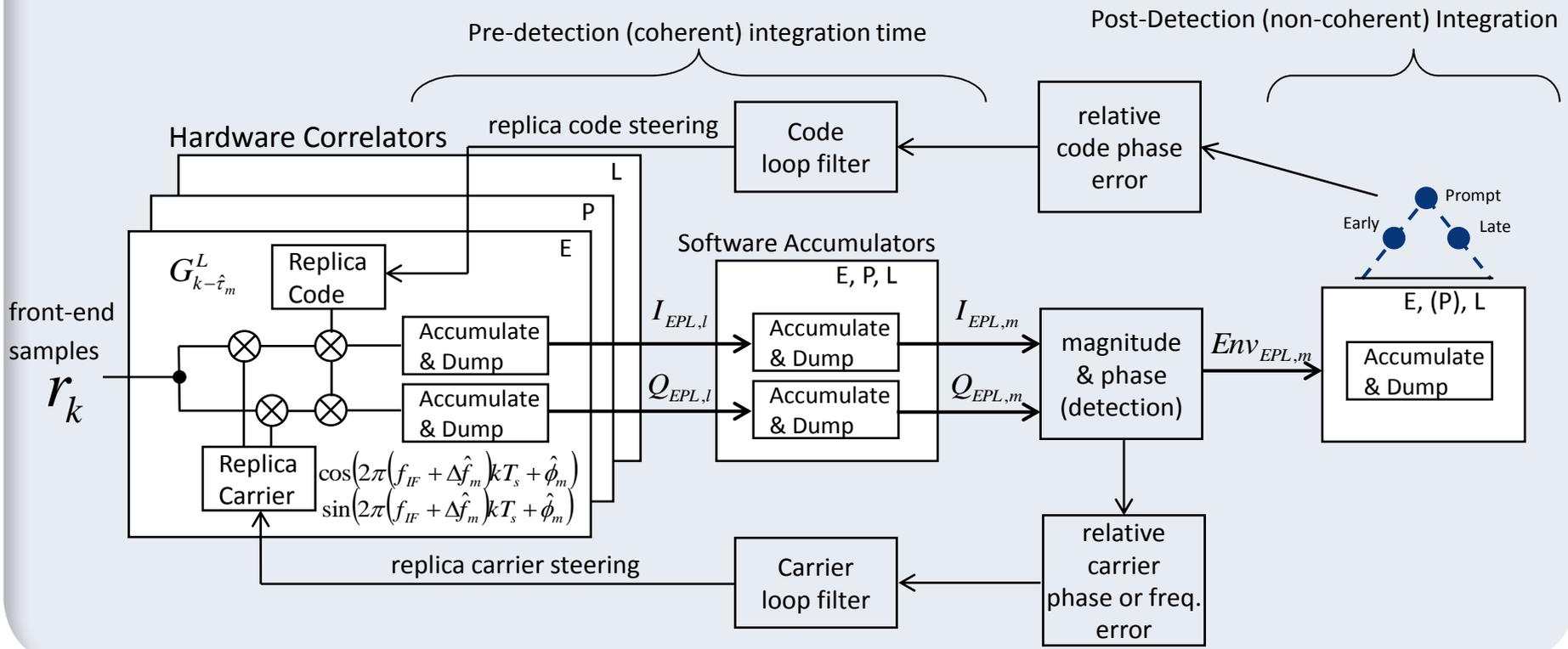
$$\sigma_{n_0}^2 = -130 \text{ dBW}$$

$$S/N_0 = -159 - (-130) = -29 \text{ dB}$$

$$C/N_0 = S/N_0 * B = -29 + 10 \text{Log}(B) = 43.8 \text{ dB-Hz}$$

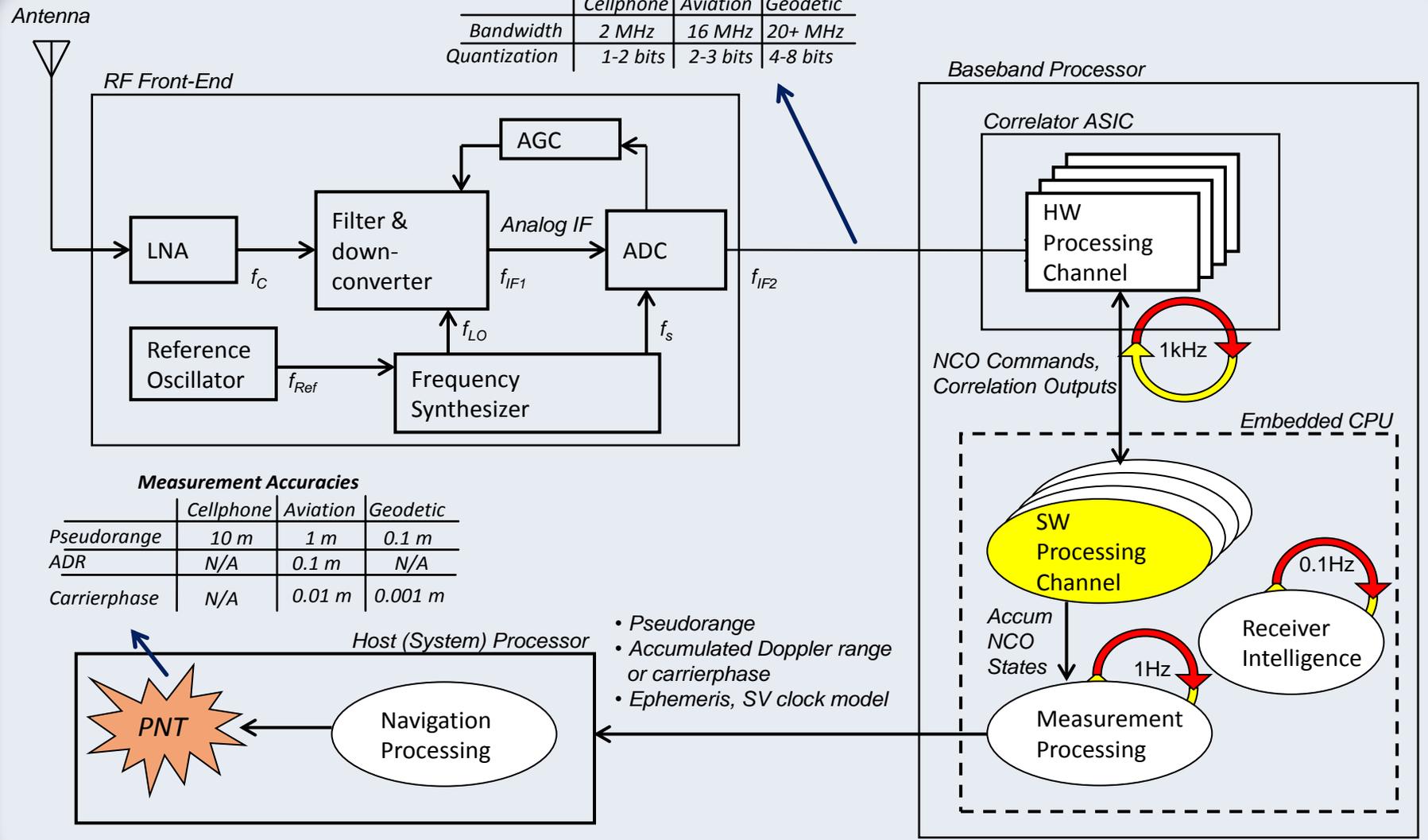
Received GNSS Signals are
~1000 times below the
noise floor!

- A GNSS receiver never actually ‘sees’ the signal. It can only estimate signal parameters relative to its replica using correlation
 - Signal’s code phase error relative to replica code
 - Signal carrier frequency or phase error relative to replica carrier
- Steering commands used to keep the replicas aligned to the signal are used to form range measurements



Generic GNSS Receiver Architecture

| | Cellphone | Aviation | Geodetic |
|--------------|-----------|----------|----------|
| Bandwidth | 2 MHz | 16 MHz | 20+ MHz |
| Quantization | 1-2 bits | 2-3 bits | 4-8 bits |



Measurement Accuracies

| | Cellphone | Aviation | Geodetic |
|--------------|-----------|----------|----------|
| Pseudorange | 10 m | 1 m | 0.1 m |
| ADR | N/A | 0.1 m | N/A |
| Carrierphase | N/A | 0.01 m | 0.001 m |

- Pseudorange
- Accumulated Doppler range or carrierphase
- Ephemeris, SV clock model

- Mass Market/Cellphone
 - Single Frequency (centered between GPS L1 and GLONASS L1 bands)
 - Size and cost are highest priority
 - Designs: helical SMT (linearly polarized), quadrifilar or chip (RHCP)
 - Size: <2 cm, Cost: <\$ 3
- Aviation/Machine Control
 - Single or dual frequency
 - L1/L2 for high-accuracy industrial
 - L1/L5 for aviation
 - Patch antenna design with built-in diplexer and LNA
 - Low-elevation cutoff using planer designs and absorber materials
 - Phase center stability controlled by design
 - Size: ~10 cm, Cost: \$20-300
- Geodetic/Reference Station
 - Supports multiple GNSS bands
 - Supports PPP network bands (e.g. TerraStar)
 - Similar design criteria as high-end Aviation/Machine control antennas
 - Excellent phase center stability over azimuth and GNSS bands
 - Choke ring or other 'external' multipath limiting features
 - Qualification tested
 - Size: ~30 cm, Cost \$2,500-7,000

Helical SMT, Quadrifilar, and Chip Antennas



Source: www.gsm-modem.de/M2M/m2m-componets/gps-helical-antenna/



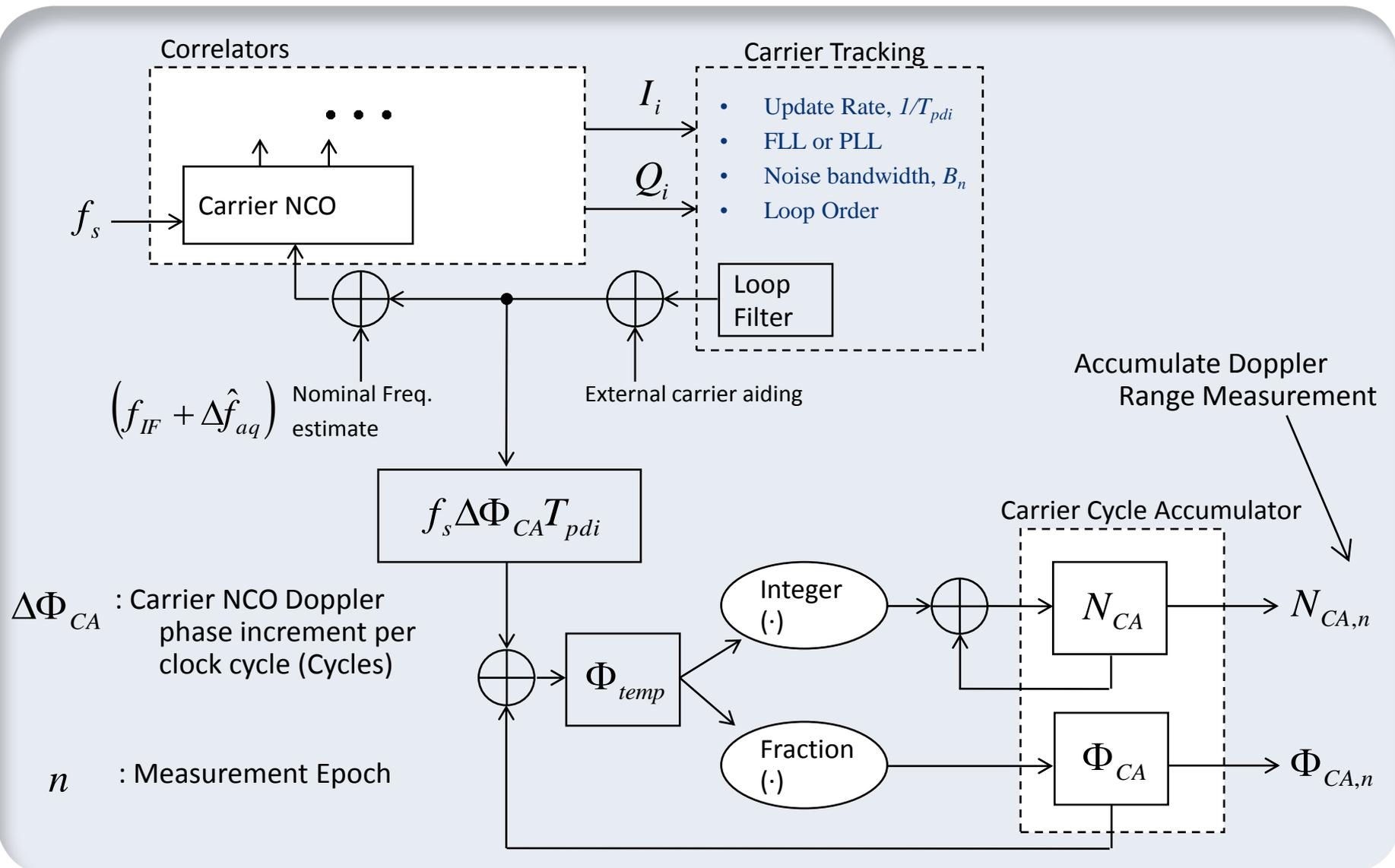
Source: Garmin



Source: NovAtel

- Desired Measurements:
 - Absolute LOS range to each visible satellite
 - Precise LOS velocity to each visible satellite
- What you get instead:
 - Pseudorange to each visible satellite
 - Noisy (1-10 meters error)
 - Absolute and unambiguous range measurement
 - Has a range bias common to all measurements of all visible satellites
 - Accumulated (integrated) Doppler Frequency Range
 - Receiver tracking carrier in frequency-locked mode
 - Robust against high dynamics, interference, multipath fading and iono scintillation
 - Decimeter-level noise
 - Relative range measurement
 - Accumulated Doppler Phase Range (a.k.a. CarrierPhase)
 - Receiver tracking carrier in phase-locked mode
 - More susceptible to loss-of-lock
 - Slips cycles can occur when tracking loop can't keep up with dynamics
 - Millimeter-level noise
 - Relative range measurement. Contains integer cycle ambiguity ($N\lambda$)

Carrier Cycle Accumulator



Pseudorange to satellite i at measurement epoch n :

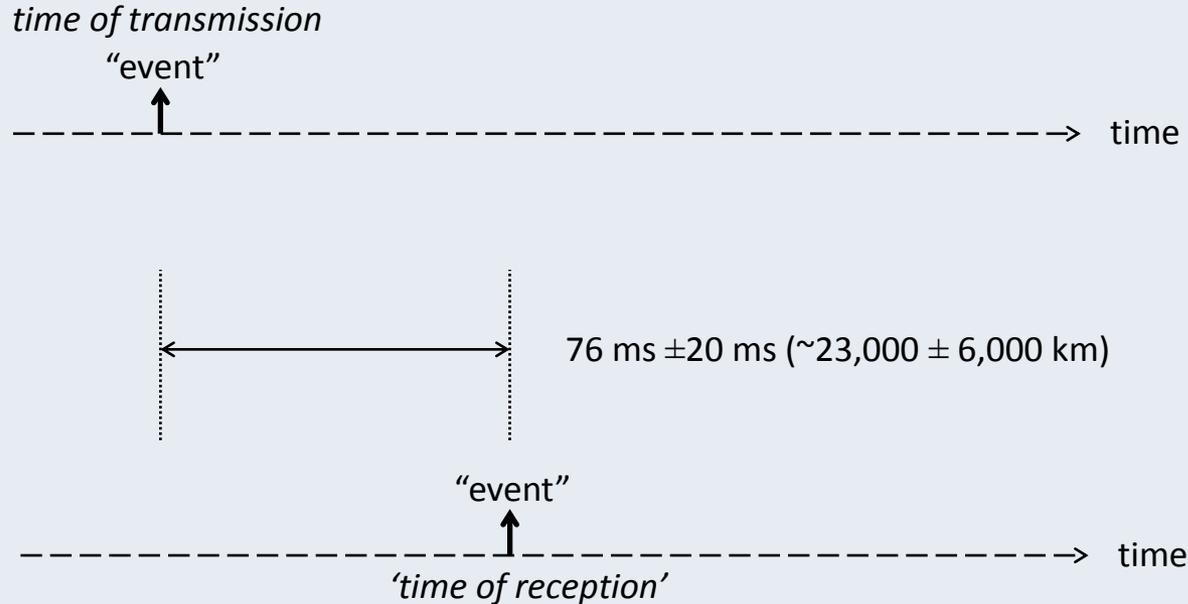
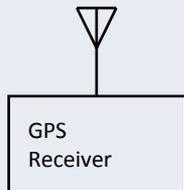
$$\rho_{i,n} = c [t_{R,n} - t_{T,i,n}] \text{ (m)}$$

Where:

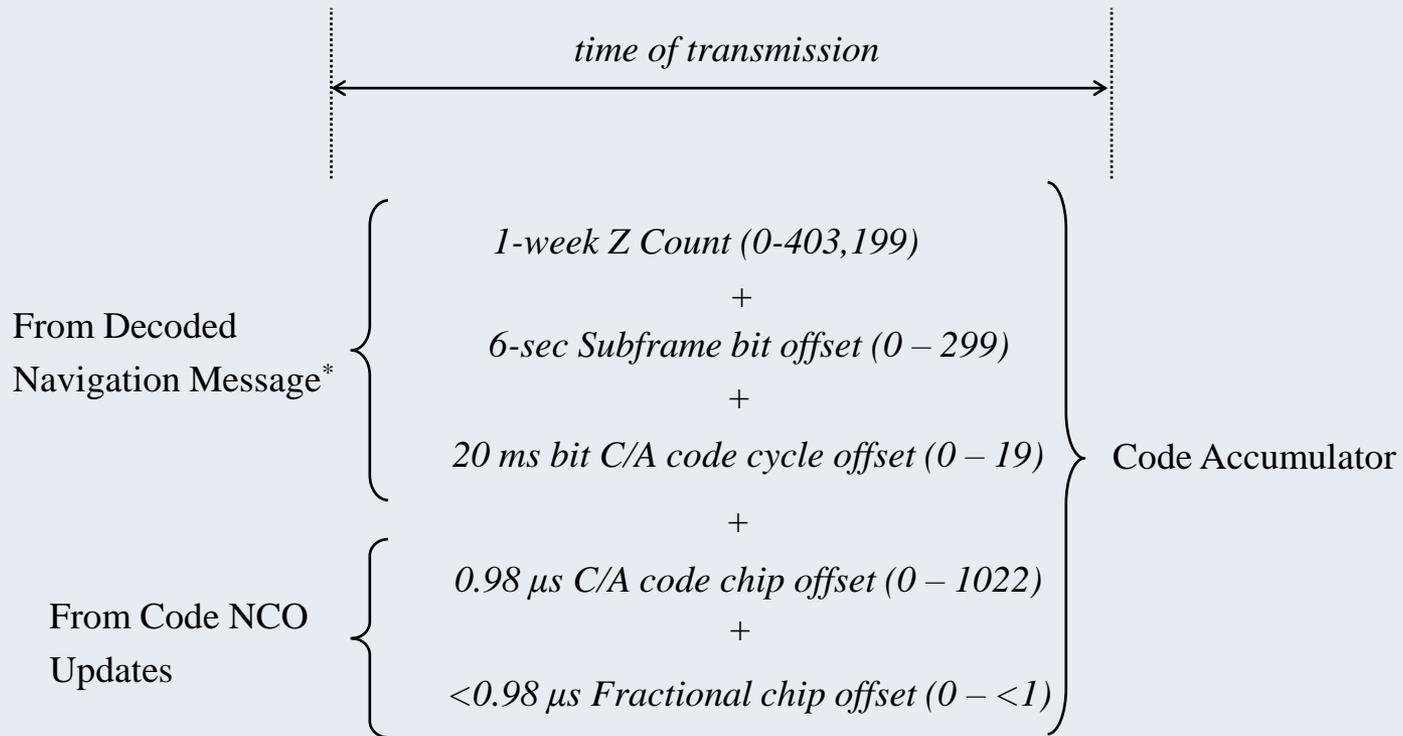
t_R : Time of reception (derived from receiver clock)

t_T : Time of transmission

c : speed of light (2.99792458×10^8 m/s)

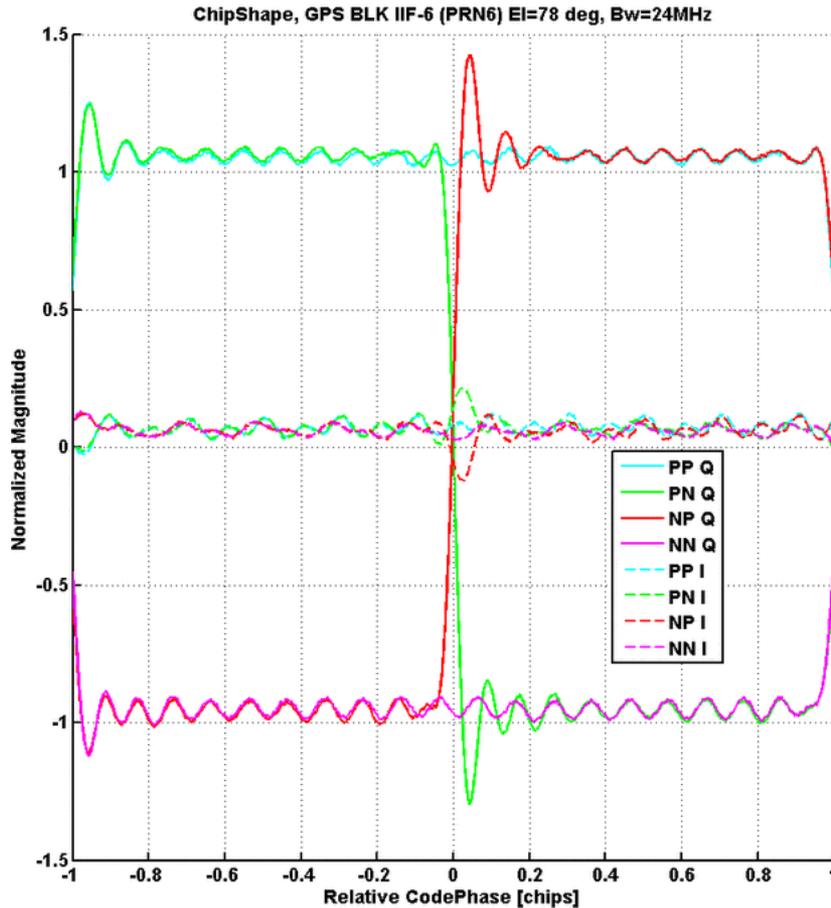


Computing Time of Transmission



* Refer to IS-GPS-200

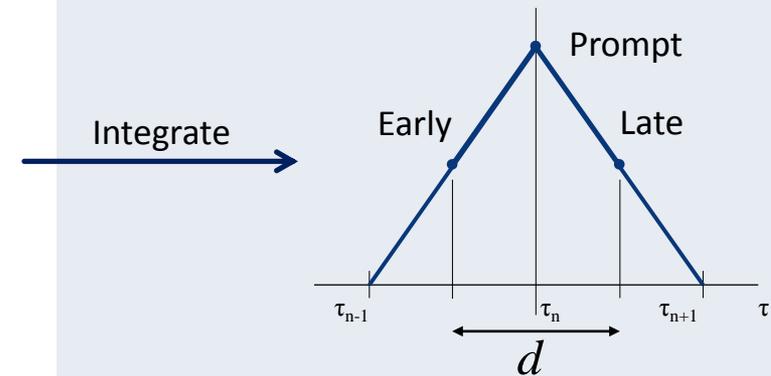
Chip Shapes of Actual GPS-SPS Signals



Time is estimated from chip transition zero crossings*

Sharp edges ↔ precise measurements

* In practice, the receiver implements an early-minus-late discriminator function



Pseudorange Measurement Accuracy

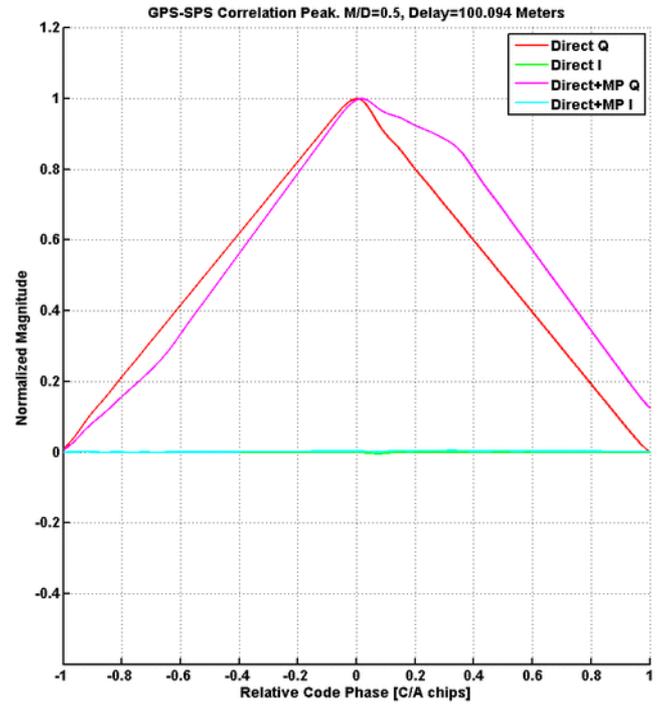
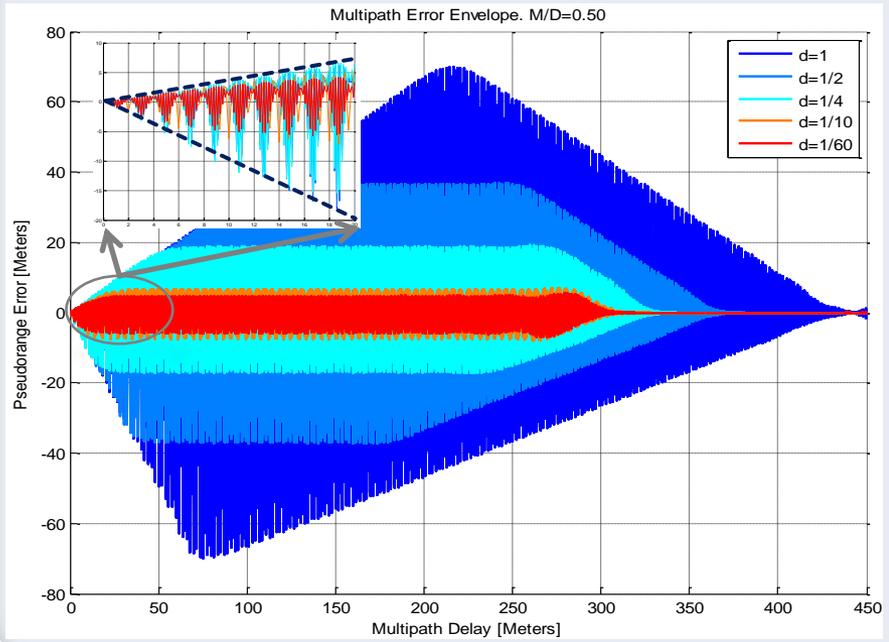
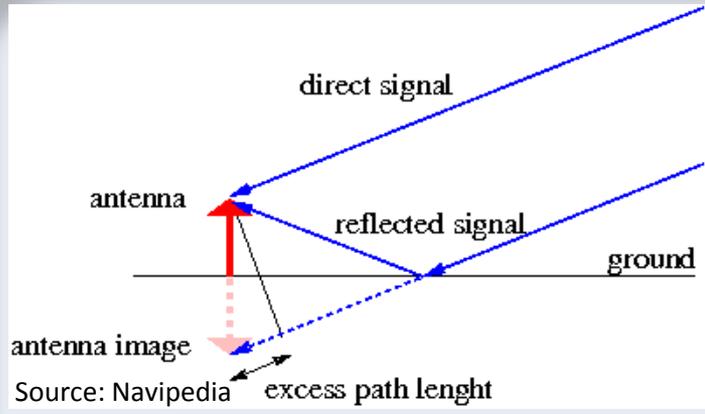
$$\sigma_{iDLL, chips} \cong \sqrt{\frac{B_n}{2C/N_0} \left(\frac{1}{B_{fe} T_c} \right) \left[1 + \frac{1}{T_{pdi} C/N_0} \right]} \quad D \leq \frac{R_c}{B_{fe}}$$

R_c : code chipping rate T_c : chip period

B_{fe} : front-end bandwidth B_n : loop noise bandwidth

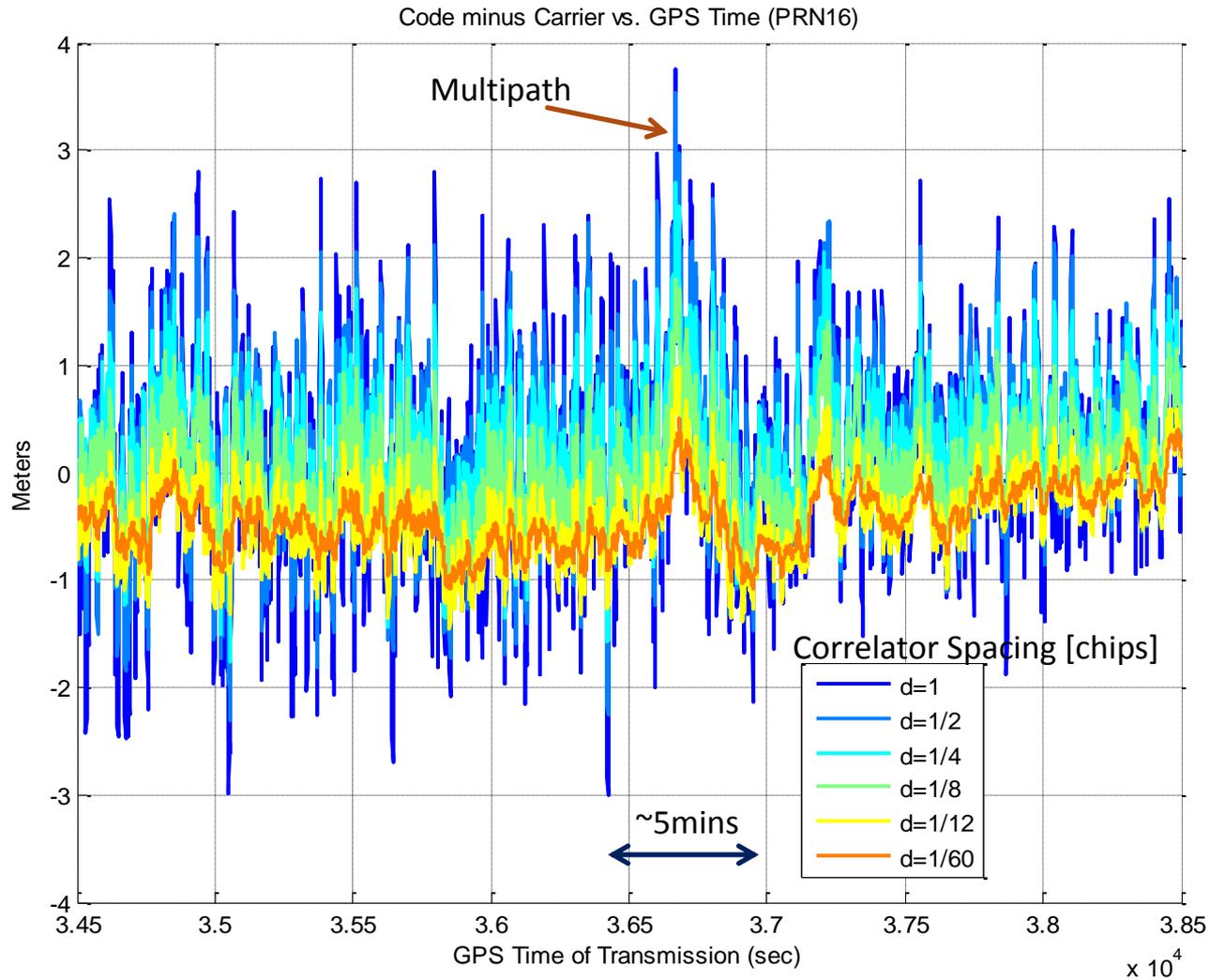
T_{pdi} : pre-detection integration time

- P. Fenton, J. Jones, "The Theory and Performance of NovAtel Inc.'s Vision Correlator," ION GNSS 2005
- S. Gunawardena, "A Universal Software Receiver Toolbox for Education and Research," InsideGNSS, July/August 2014.

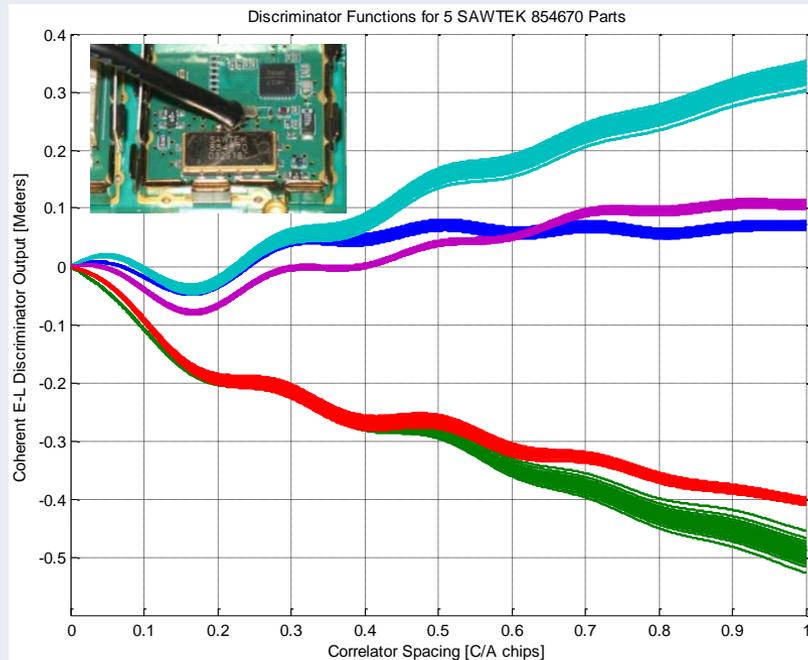


- Narrowing correlator spacing reduces the effect of correlation peak distortion due to multipath
- Also reduces code measurement error since thermal noise on E and L become correlated (but reduces tracking threshold)
- To reduce EL spacing, need sufficient bandwidth to prevent top-rounding of correlation function
- More advanced techniques in use: double-delta, MEDLL, NovAtel Vision™ Correlator
- Mitigating short-delay multipath (<3m) is still challenging

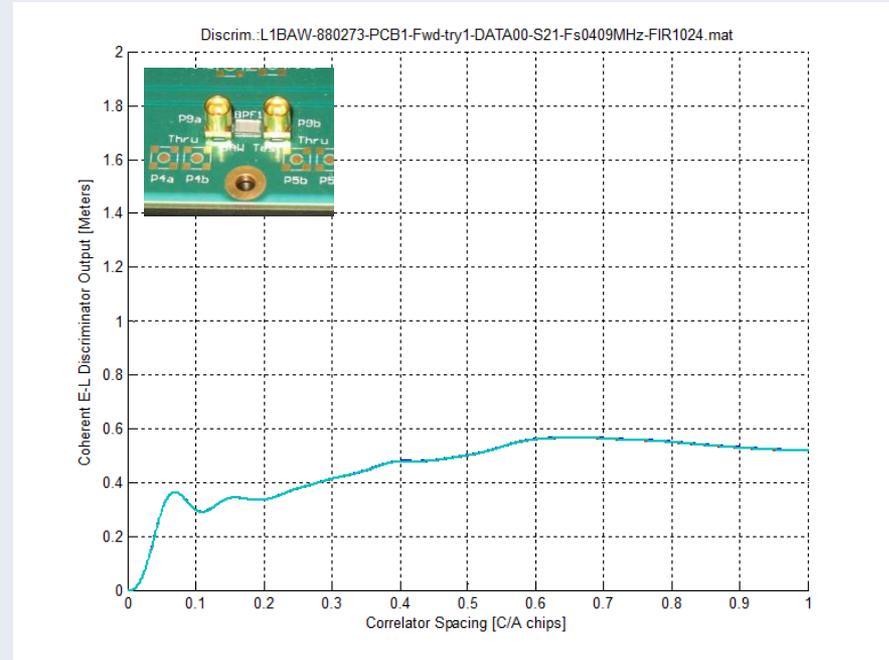
Example: Correlator Spacing, Pseudorange Accuracy & Multipath Mitigation Performance



Surface Acoustic Wave (SAW) IF Filter



Block Acoustic Wave (BAW) RF Filter



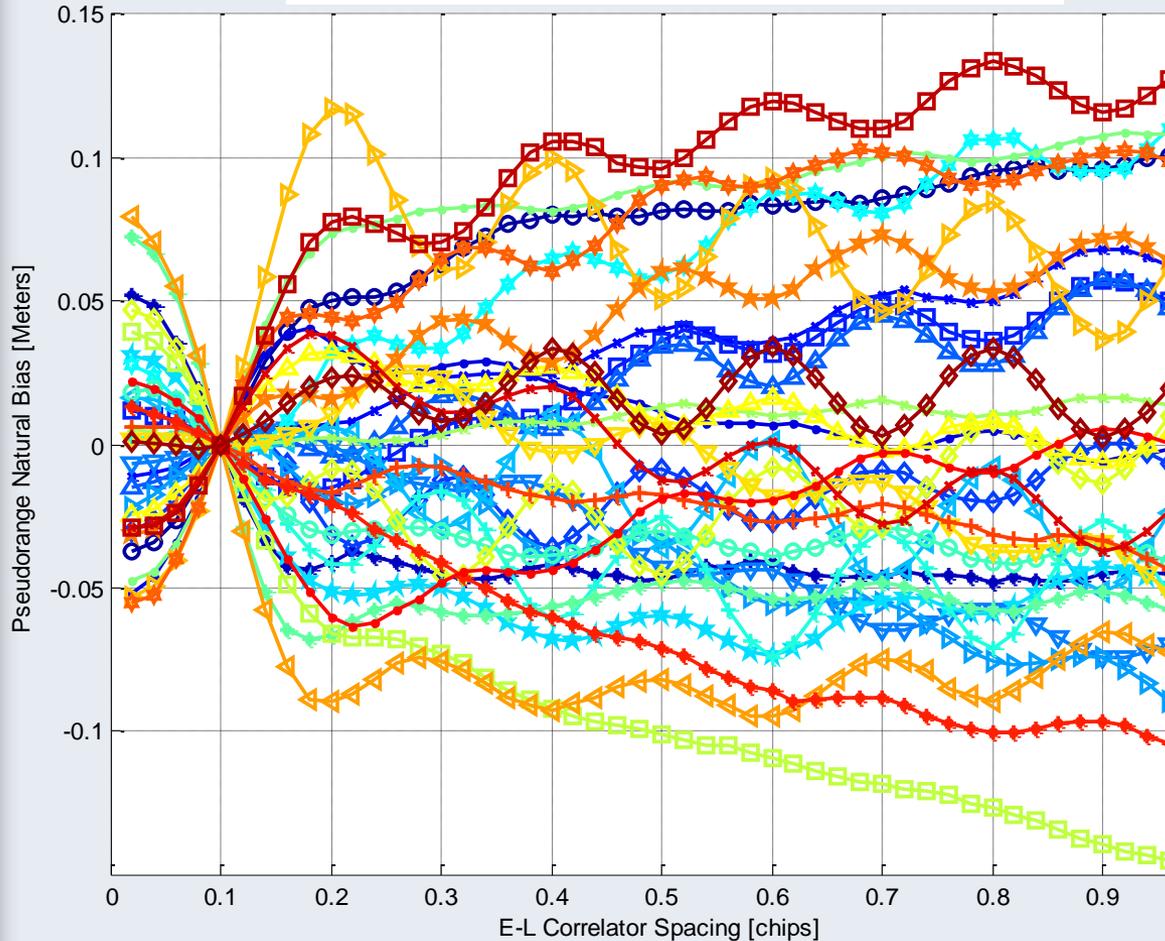
Pseudorange Variations:

~15 cm @ 0.1 chip, ~35 cm @ 0.3 chip

~20 cm @ 0.1 chip, ~70 cm @ 0.3 chip

- Impacts precision time/time transfer receivers and FDMA signals (GLONASS)
- Geodetic-grade receivers perform in-system calibration for GLONASS FDMA
- IF SAW filters can induce cm-level inter-PRN pseudorange biases

GPS-SPS Pseudorange Natural Biases



- PRN01, SV63, Block IIF, El:57, Pdi:400s
- ◆ PRN02, SV61, Block IIR, El:69, Pdi:210s
- PRN03, SV33, Block IIA, El:69, Pdi:400s
- ◆ PRN04, SV34, Block IIA, El:82, Pdi:390s
- PRN05, SV50, Block IIR-M, El:87, Pdi:390s
- ◇ PRN06, SV36, Block IIA, El:58, Pdi:450s
- △ PRN07, SV48, Block IIR-M, El:88, Pdi:1000s
- ▽ PRN08, SV38, Block IIA, El:77, Pdi:1000s
- △ PRN09, SV39, Block IIA, El:53, Pdi:600s
- △ PRN10, SV40, Block IIA, El:68, Pdi:480s
- ★ PRN11, SV46, Block IIR, El:57, Pdi:730s
- ★ PRN12, SV58, Block IIR-M, El:49, Pdi:300s
- ✦ PRN13, SV43, Block IIR, El:64, Pdi:440s
- PRN14, SV41, Block IIR, El:68, Pdi:1150s
- ◆ PRN15, SV55, Block IIR-M, El:79, Pdi:1510s
- ◆ PRN16, SV56, Block IIR, El:88, Pdi:650s
- ◆ PRN17, SV53, Block IIR-M, El:69, Pdi:980s
- PRN18, SV54, Block IIR, El:76, Pdi:750s
- ◇ PRN19, SV59, Block IIR, El:71, Pdi:780s
- △ PRN20, SV51, Block IIR, El:41, Pdi:850s
- ▽ PRN21, SV45, Block IIR, El:79, Pdi:1560s
- ▽ PRN22, SV47, Block IIR, El:88, Pdi:1270s
- △ PRN23, SV60, Block IIR, El:75, Pdi:450s
- ★ PRN24, SV65, Block IIF, El:53, Pdi:780s
- ★ PRN25, SV62, Block IIF, El:44, Pdi:400s
- ✦ PRN26, SV26, Block IIA, El:57, Pdi:610s
- ◆ PRN28, SV44, Block IIR, El:80, Pdi:500s
- ◆ PRN29, SV57, Block IIR-M, El:64, Pdi:1210s
- ◆ PRN30, SV35, Block IIA, El:84, Pdi:1290s
- PRN31, SV52, Block IIR-M, El:77, Pdi:450s
- ◇ PRN32, SV23, Block IIA, El:60, Pdi:720s

cm-level errors for differential GPS users using dissimilar receivers

Antenna and Front-End Comparison

| Receiver Type → Design Parameters ↓ | Mass Market / Consumer | Aviation Grade / Machine Control | Geodetic / Reference Station |
|---|---|--|---|
| Antenna Type Coverage Bands Approximate Size | Passive chip or helical element Covers L1 bands (GPS, GLONASS) Surface Mount Package <2cm  | Patch on controlled dielectric single element (L1 band) or Stacked (L1 and L1/L5 bands) Integrated diplexer and LNA 10 cm  | Multipath Limiting Elements Stable Phase Center External Choke Ring Design In-system calibration of inter-channel biases 30 cm  |
| GNSS Bands | GPS L1 C/A, and GLONASS L1 and/or BeiDou B1 SBAS on L1 | GPS L1 C/A GPS L5 SBAS on L1 and L5 | GPS L1 C/A, P(Y)* GPS L2 C, P(Y)* GPS L5 |
| Pre-correlation Bandwidths | <2MHz (GPS C/A) <2 MHz (GLONASS) | 4-16 MHz (L1) 16 MHz (L5) | 16-24 MHz (L1, L2, L5) |
| Sample quantization and effective sample data rate (Mbytes/sec) | 1 or 2 bits/sample 0.5-1.0 | 2-4 bits/sample 8-32 | 2-8 bits/sample 24-150 |
| Pre-Correlation Interference Detection/Suppression | none | CW, Swept CW, FM Non-uniform quantization J/N meter | Pulse-suppression, notch filter, frequency-domain excision |
| Reference Oscillator Type and stability | TCXO ($\leq 10^{-6}$) | High-performance TCXO or OCXO ($10^{-6} - 10^{-7}$) | OCXO or atomic standard (10^{-9}) |

* Using codeless or semi-codeless tracking techniques

Baseband Processing Comparison

| Receiver Type → Design Parameters ↓ | Mass Market / Consumer | Aviation Grade / Machine Control | Geodetic / Reference Station |
|--|--|--|--|
| Carrier Tracking Architecture | None (A-GNSS) FLL (standalone GNSS) | FLL-assisted PLL or PLL (inertial aiding) | PLL (ephemeris aiding) |
| Code Tracking Architecture | None (A-GNSS) carrier-aided DLL (standalone) | carrier-aided DLL | carrier-aided DLL |
| Multipath Mitigating Technology | none | Narrow-correlator Double-delta correlator Vision™ Correlator | Narrow-correlator Double-delta correlator Vision™ Correlator |
| Typical Early-Late Correlator Spacing (GPS L1 C/A Chips) | 1.0 | 0.3-0.1 | 0.1-0.01 |
| Inter-Channel Pseudorange Bias Correction (Primarily for GLONASS) | None OR Model-wide calibration table | Device-specific calibration table (part of device testing and qualification process) | Dynamic calibration |
| Other features | Massive banks of parallel correlators for 'flash acquisition and long coherent integration | Dynamic multipath estimation and mitigation (e.g. NovAtel Vision™ correlator) | Interference and signal deformation monitoring |
| Typical Implementation (2014) | System on chip (SOC) ASIC with integrated RF and baseband (standalone) | 2-ASICs (RF + Baseband) Single SMD module or card | Front-end: RFIC-based Baseband: ASIC or FPGA + embedded processor |
| Power consumption and Cost | <2 W < \$3 | <20W \$300-\$3,000 | >30W \$6000-30,000 |

Ask the Experts – Part 1



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Sandy Kennedy
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Poll #2

What accuracy would you like to get in the future?

- *Greater than a meter*
- *Less than a meter*
- *Meter*
- *10 centimeters*
- *Less than 10 centimeters*

Software processing requirements for precise positioning



Sunil Bisnath
Associate Professor
York University

Performance

Quality and types
of measurements

Antenna
Receiver

Error
modeling

Long list

Positioning
mode

Point positioning
Relative positioning
DGNSS
RTK / Network RTK
PPP

- Continuous L1 C/A-code measurements ...
- From minimum of 4 GPS (GNSS) satellites ...
- To compute user 3D position and receiver timing error.
- Perhaps: use of L1 carrier phase + filtering
- Quality of L1 C/A-code measurements: ~ 1 m + noise

Mode of operation for $\sim 99\%$ of users

- Receiver
- Additional infrastructure
- Communication link
- Measurement corrections
- Data processing

- High-performance (geodetic)
- L1 C/A-code tracking (+ L1 P(Y)-code) + L1 carrier-phase
- + L2 P(Y)-code + L2 carrier-phase
- P(Y)-code tracking at 10s cm + noise
- Carrier-phase tracking at mms + noise

- A second receiver, or ...
- Working within a network of receivers and receiving additional GNSS signals and corrections, or ...
- Receiving additional corrections

Generation:

- Orbit errors
- Clock errors
- Phase wind-up
- Phase center offset
- Phase center variation
- Equipment delays

Transmission:

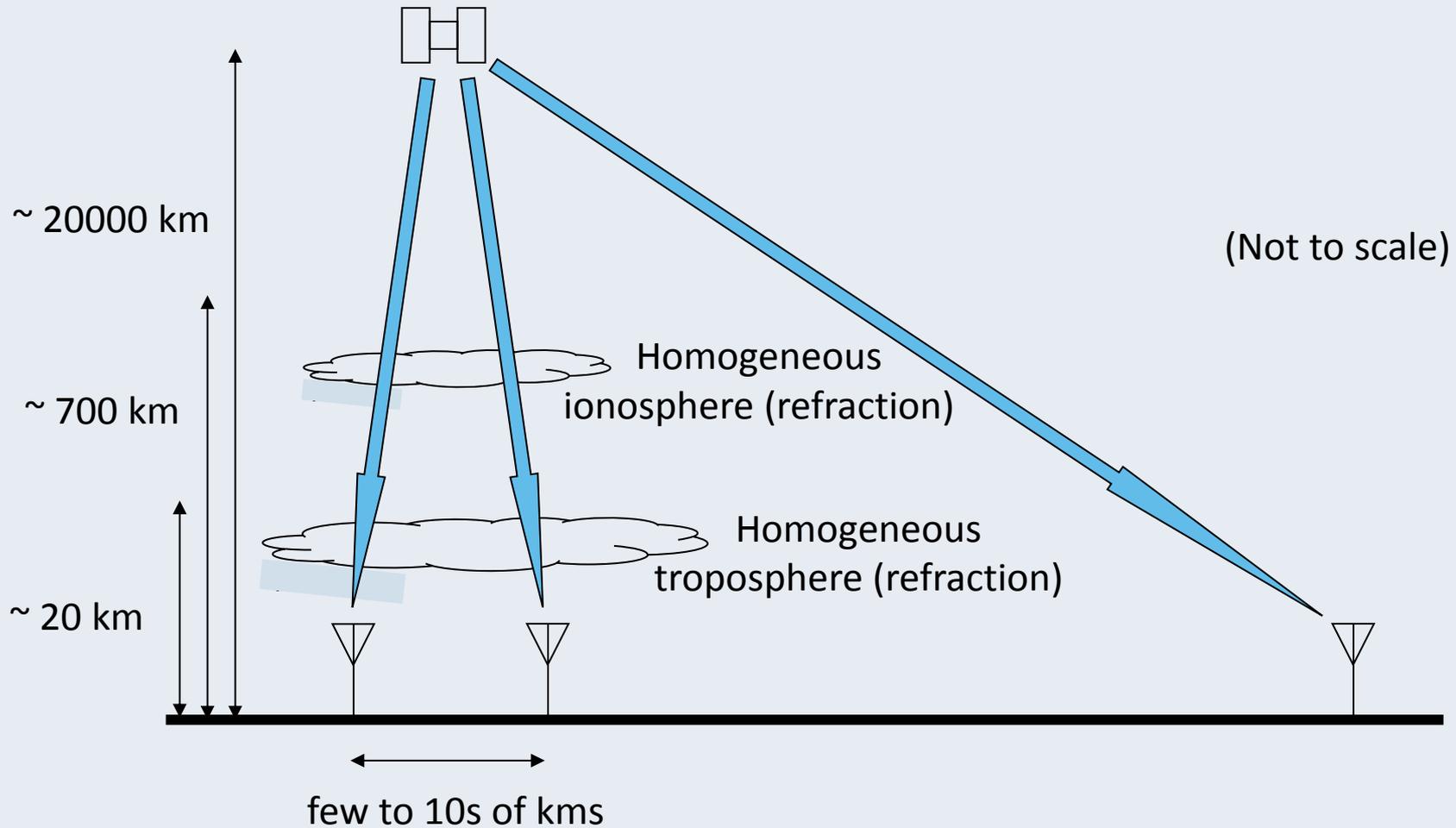
- Ionospheric refraction
- Tropospheric refraction

Reception:

- Multipath
- Phase center offset
- Phase center variation
- Phase wind-up
- Solid Earth tides
- Ocean loading
- Equipment delays
- Receiver noise

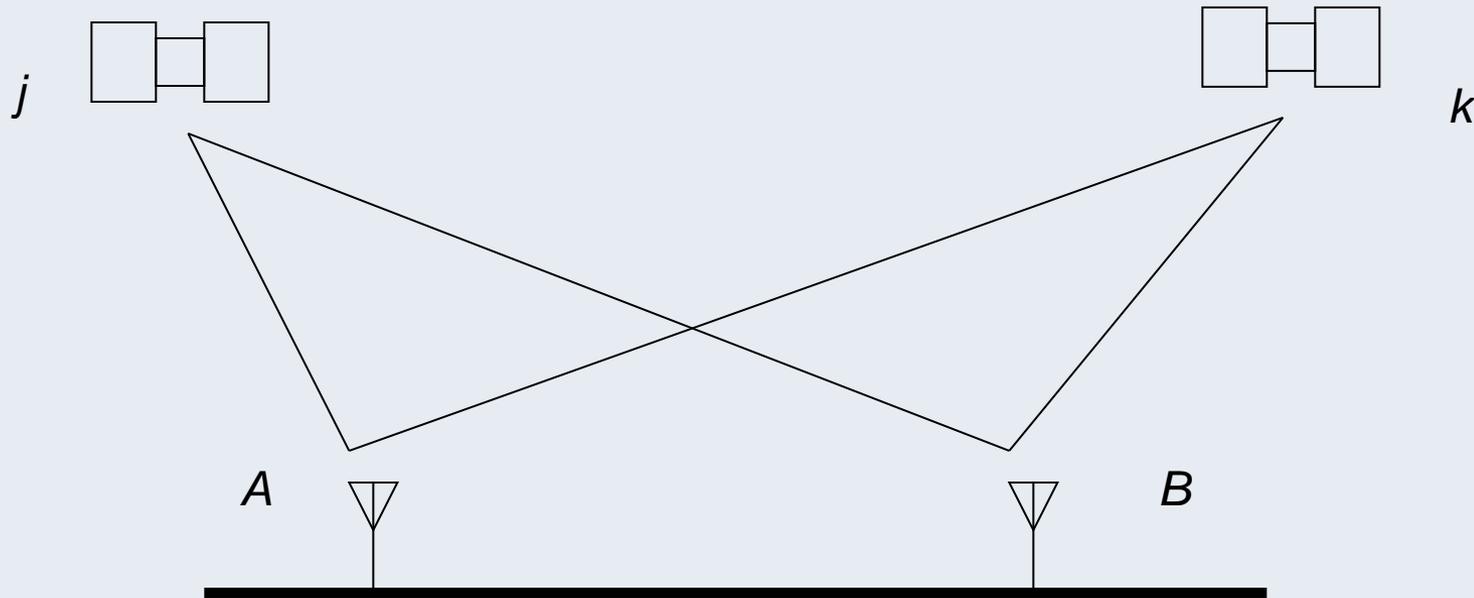
| Effect | Magnitude | Domain | Mitigation method | Residual error |
|------------------------------------|-----------|------------|--------------------------|----------------|
| <i>Ionosphere</i> | 10s m | range | linear combination | mm |
| <i>Troposphere</i> | few m | range | modelling; estimation | dm - mm |
| <i>Relativistic</i> | 10 m | range | modelling | mm |
| <i>Sat phase centre; variation</i> | m - cm | pos; range | modelling | mm |
| <i>Code multipath; noise</i> | 1 m | range | filtering | dm - mm |
| <i>Solid Earth tide</i> | 20 cm | position | modelling | mm |
| <i>Phase wind-up (iono-free)</i> | 10 cm | range | modelling | mm |
| <i>Ocean loading</i> | 5 cm | position | modelling | mm |
| <i>Satellite orbits; clocks</i> | few cm | pos; range | filtering | cm - mm |
| <i>Phase multipath; noise</i> | 1 cm | range | filtering | cm - mm |
| <i>Rcv phase centre; variation</i> | cm - mm | pos; range | modelling | mm |

Spatial Decorrelation of Errors – Atmospheric Refraction Example



- Double-difference:

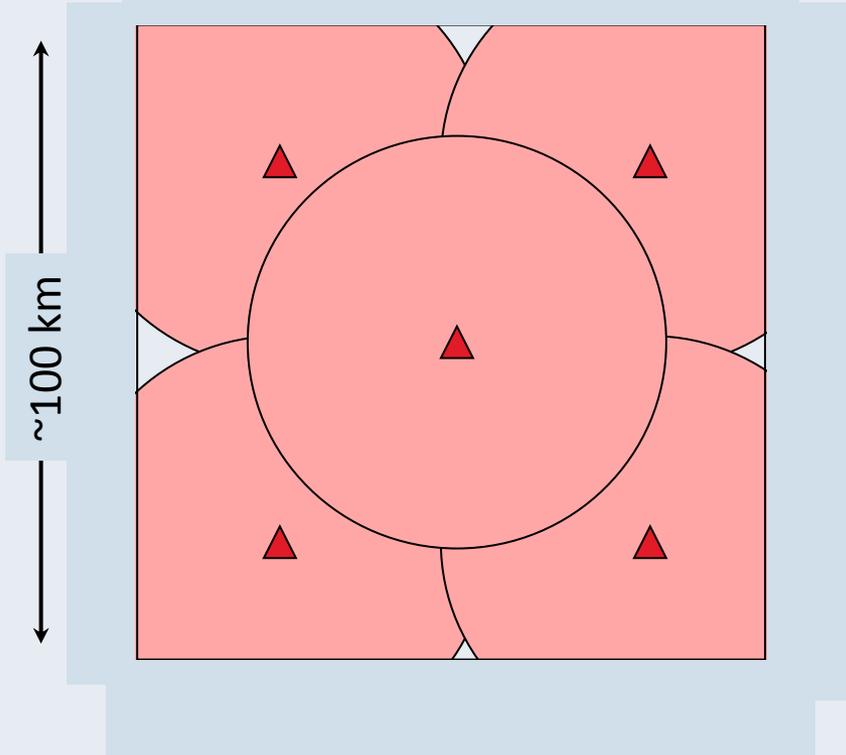
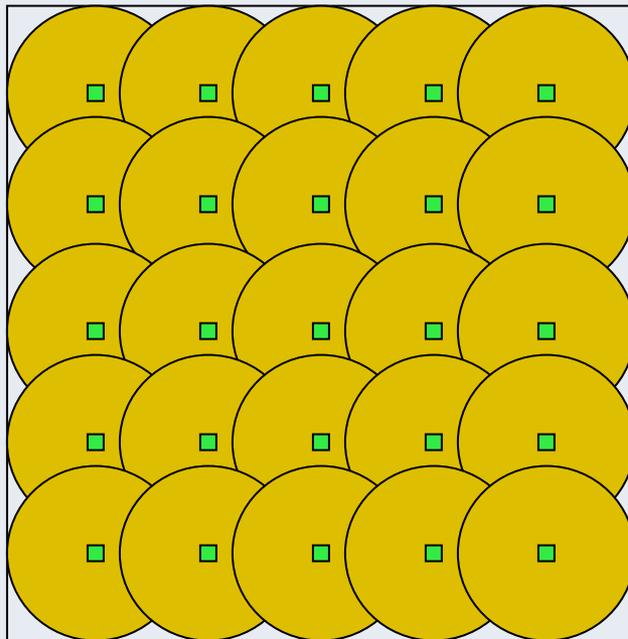
Mathematical differencing of simultaneous measurements from two satellites j and k , and from two receivers A and B



1. Generation of potential integer ambiguity candidates:
 - Is “guess” integer ambiguity for double-difference satellite pair
 - More candidates → higher probability of correct ambiguity
 - Fewer candidates → faster search
2. Identification of optimum ambiguity candidate:
 - Criterion typically integer candidate which minimizes sum of square of residuals (least-squares criterion), as optimum candidate should “best” fit data
3. Validation (or verification) of selected ambiguities:
 - Assessment of correctness of integers obtained

- Relative positioning accuracy varies depending on:
 - Length of data set (longer time spans better)
 - Single-frequency vs dual-frequency data (single-frequency greatly limited)
 - s/w: modeling of errors; ambiguity resolution
- Performance range:
 - mm-cm-level → Static relative positioning with many hours of data over hundreds to thousands of kms
 - Few cm-level → Kinematic relative positioning with seconds of data over a few kms -> *baseline RTK (Real-Time Kinematic)*

- RTK: ~25-30 reference stations per $10\,000^2$ km
- Network RTK: ~5-10 reference stations per $10\,000^2$ km



Standard Positioning Service

m-level real-time broadcast GPS orbit and clock information

+

User GPS satellite C/A-code tracking information

+

Epoch measurement filtering

=

m-level user position estimate

Precise Point Positioning

cm-level real-time or post-processed precise GPS orbit and clock information

+

User GPS satellite L1/L2 code and phase tracking information

+

Sequential measurement filtering

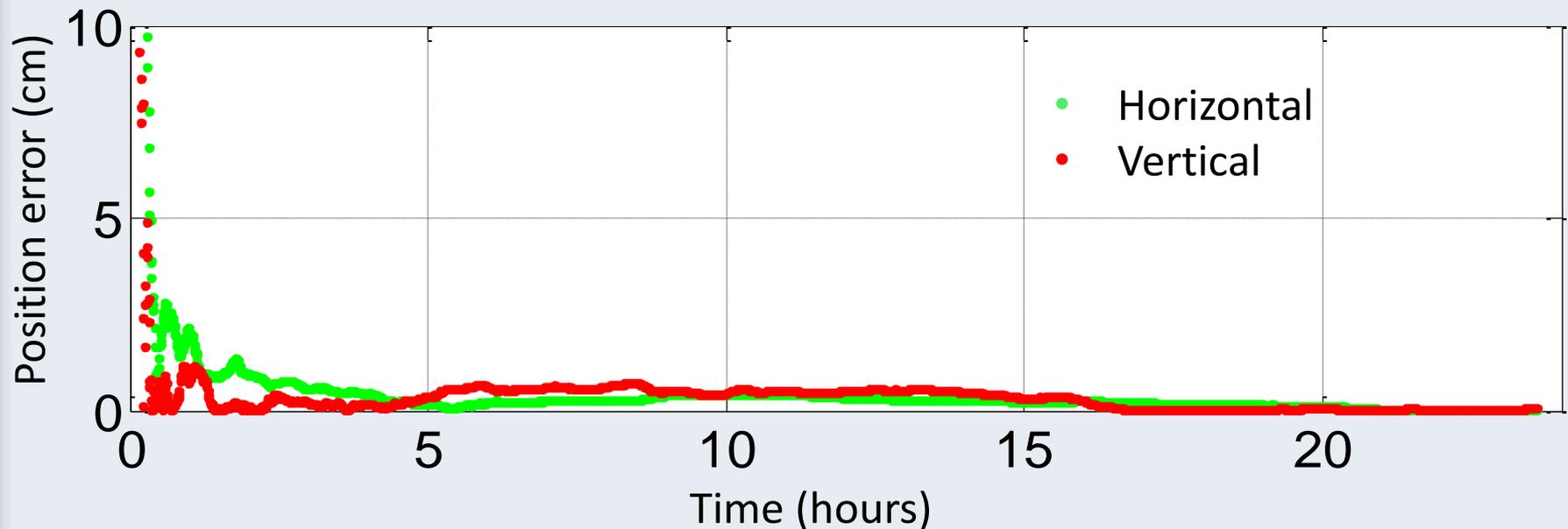
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Additional error modeling

=

dm- to mm-level user position estimate

- A good, static GPS PPP solution over 24 hours



- Characteristic PPP initial convergence period
- Solution very sensitive to quality of measurements

- RTK / network RTK mature technology → *industry standard*
- PPP is standard for high-precision, remote operation
- Infrastructure and usage continue to grow
- New GNSS signals enhancing RTK and PPP performance
 - Most network RTK services are now GPS+GLONASS
 - GPS+GLONASS PPP reduces convergence period
- Fast PPP re-convergence and PPP-AR is being commercialized
- Fast RTK-like initialization for PPP is still a goal

Practical Example

Precise Positioning Use Case



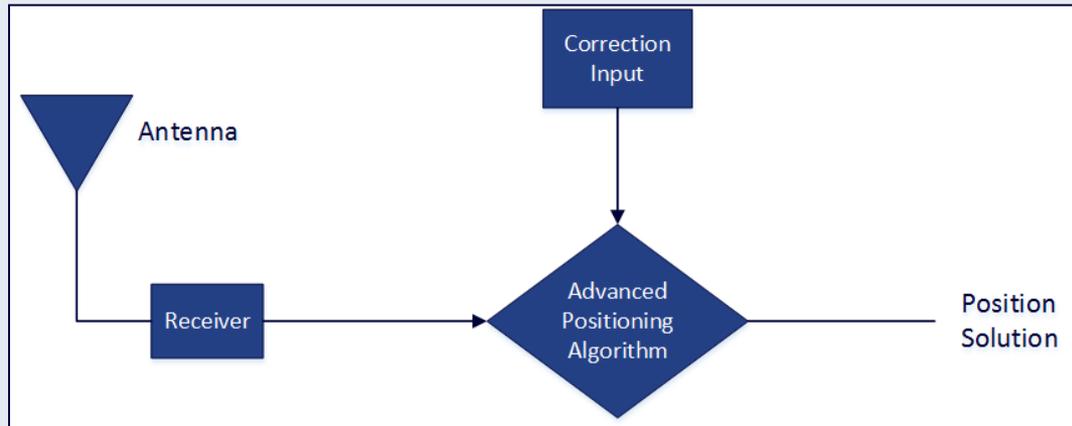
Sandy Kennedy
Director, Core Receiver Cards
NovAtel Inc.

- Positioning Accuracy Requirement:
 - <10 cm
- Correction Source:
 - TerraStar-D
- Algorithm Deployed:
 - Precise Point Positioning



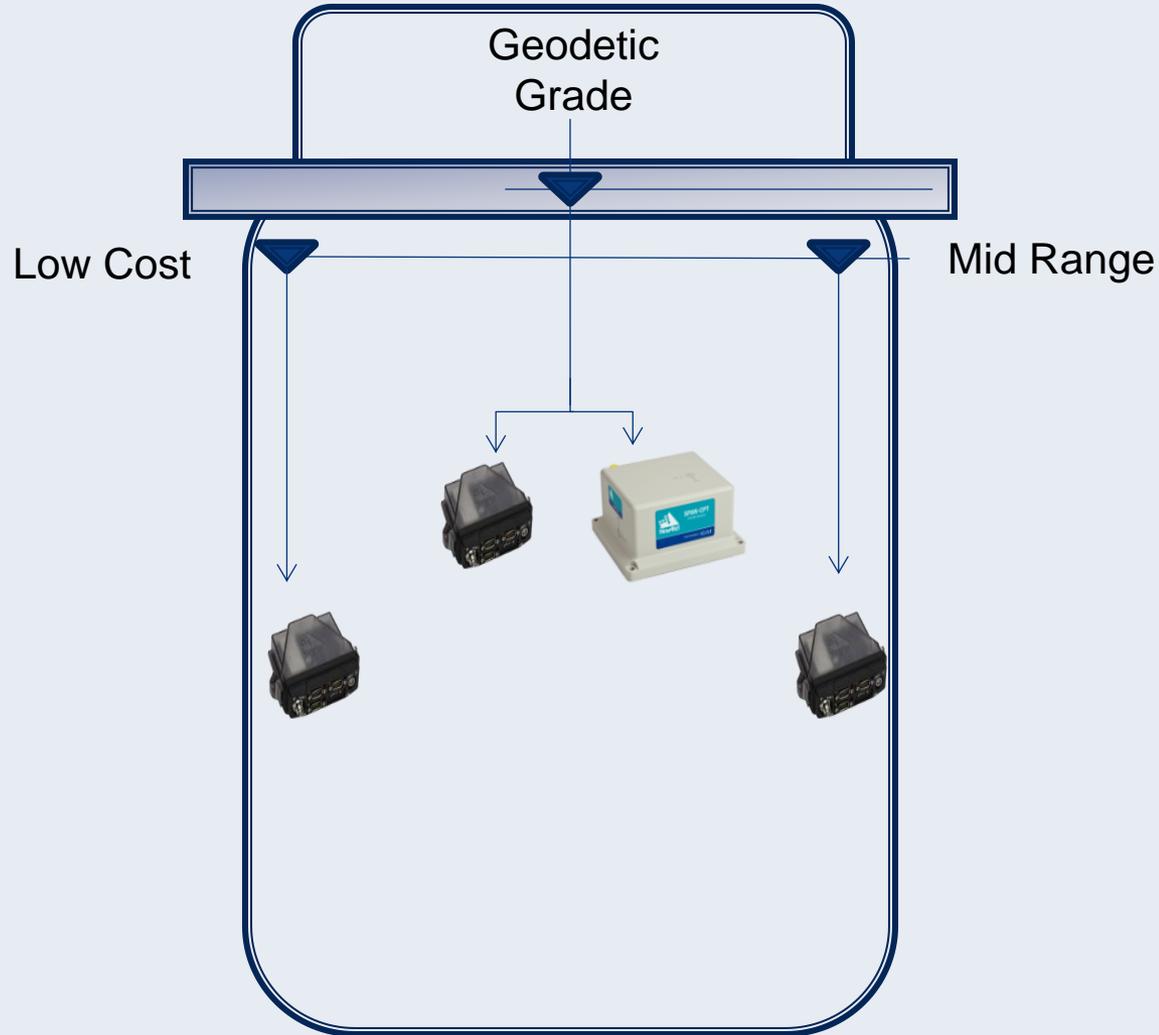
- Rationale for Choice:
 - Meets accuracy requirement
 - Primarily open sky, means good line of sight to geostationary satellite providing corrections
 - No extreme maneuvers (i.e. no barrel rolls), so should have a continuous solution

- Antenna
 - Needs to be able to receive correction signal and GPS/GLO L1/L2
 - Front door to the receiver
- Receiver:
 - Capable of tracking TerraStar-D correction signal
 - GPS/GLO L1 and L2 capable
 - Minimized multipath via Pulse Aperture Correlator technology
 - PPP engine on board



- Antennas are often taken for granted
- Often viewed as a cost saving opportunity

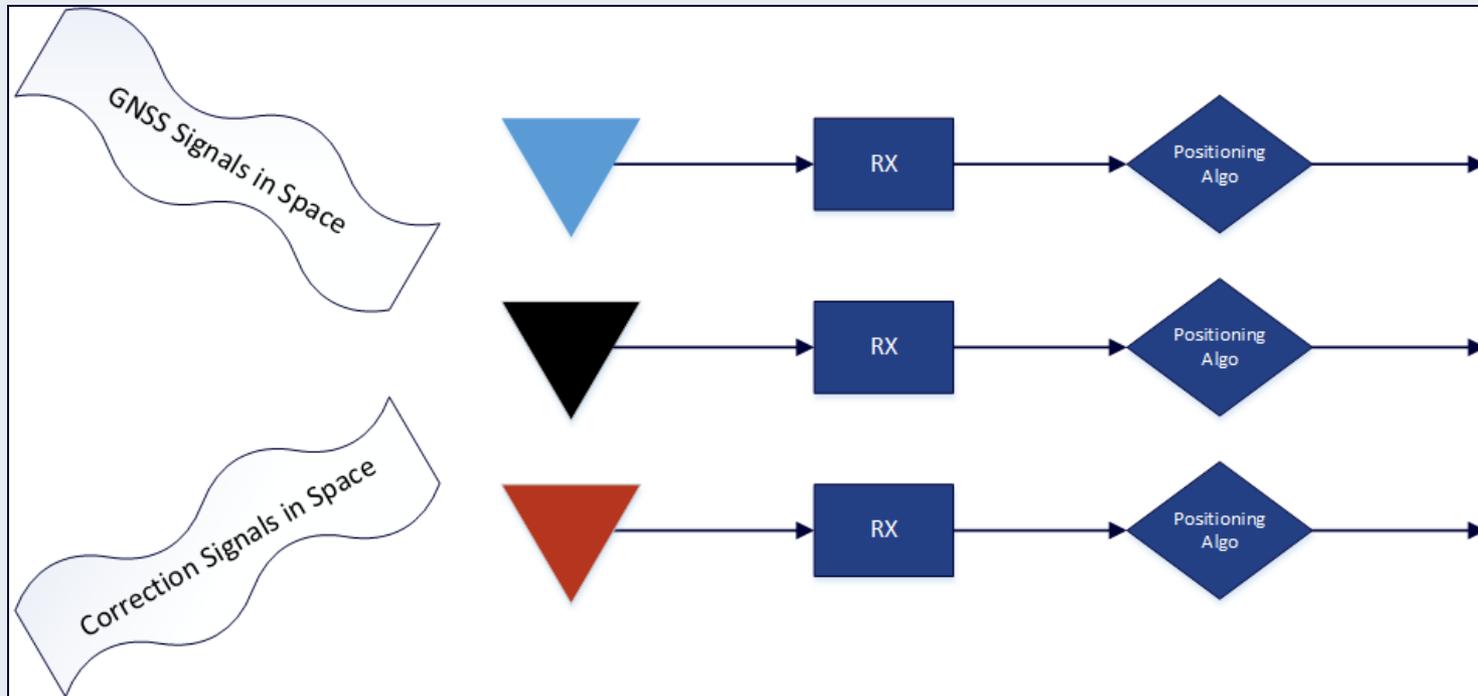
- 3 antenna choices
 - Top quality, “geodetic grade” antenna
 - Mid-range antenna, still good quality but some design compromises
 - Low-cost antenna that claims to support all necessary frequencies:
 - Correction signal = 1525-1550 MHz
 - GPS L1 = 1575.42 MHz
 - GPS L2 = 1227.60 MHz
 - GLO L1 = 1601.66 MHz (centre)
 - GLO L2 = 1245.73 MHz (centre)



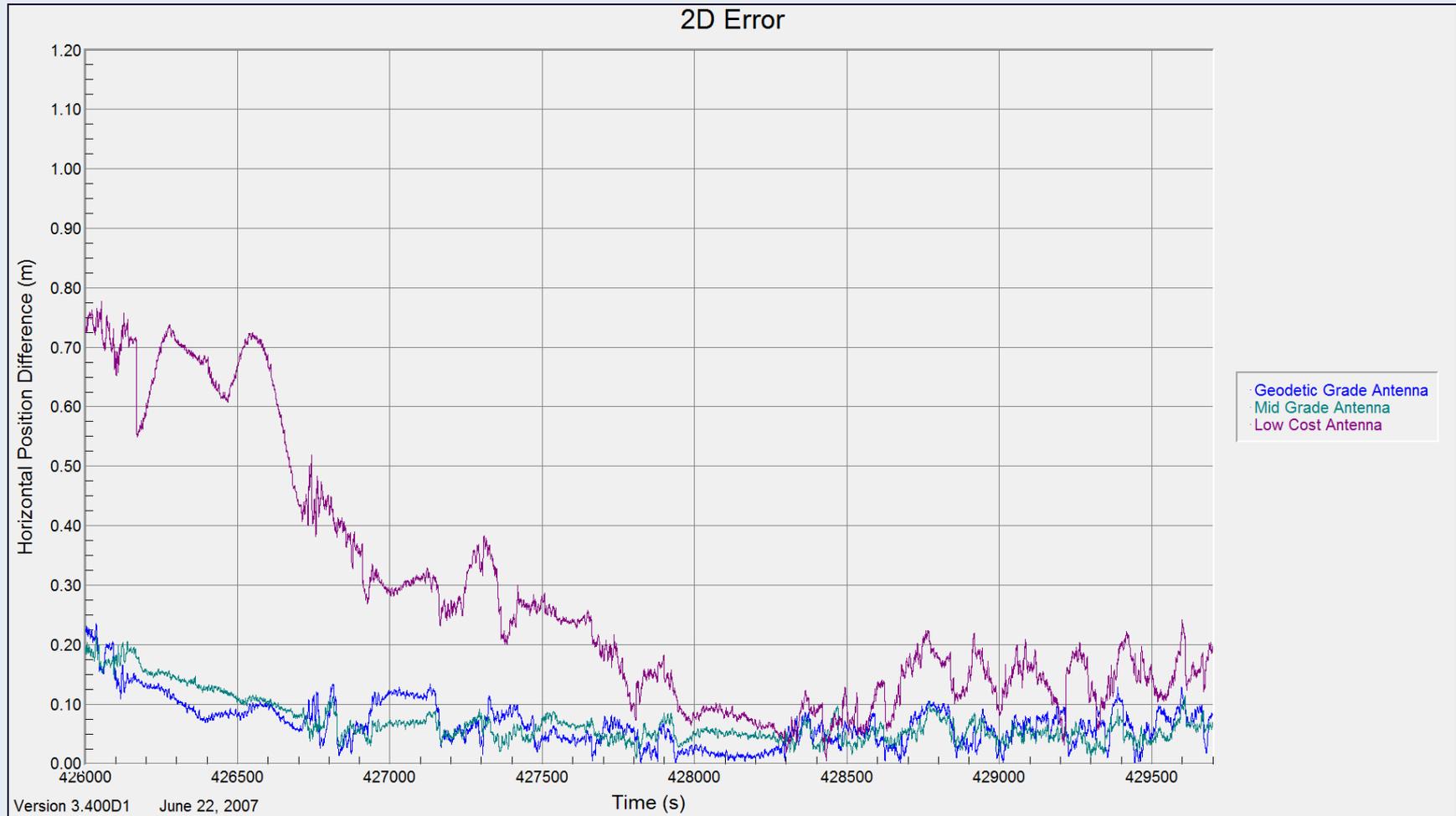
- Reference system:
 - SPAN GNSS/INS with own antenna, post processed for best accuracy solution
 - Provides attitude
 - Measured offset vectors (lever arms) between reference antenna and test antennae
- Position errors measured by moving the reference solution to each Unit Under Test location and differencing the reference and UUT trajectories
- Drove a route with a good clear sky view

- Same signals in space
- Same receiver model
- Same algorithm

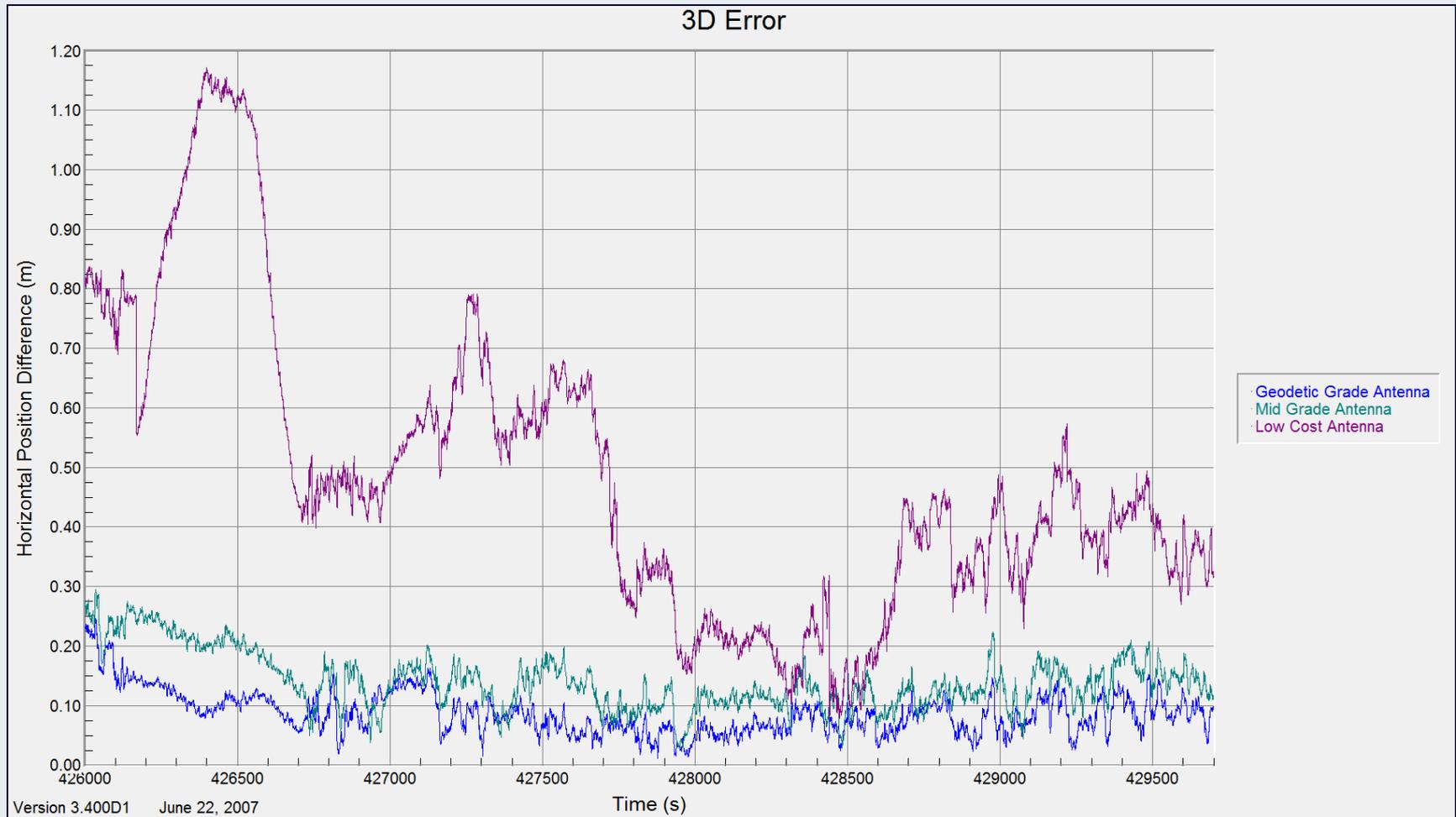
- Only difference is the antenna



2D Error

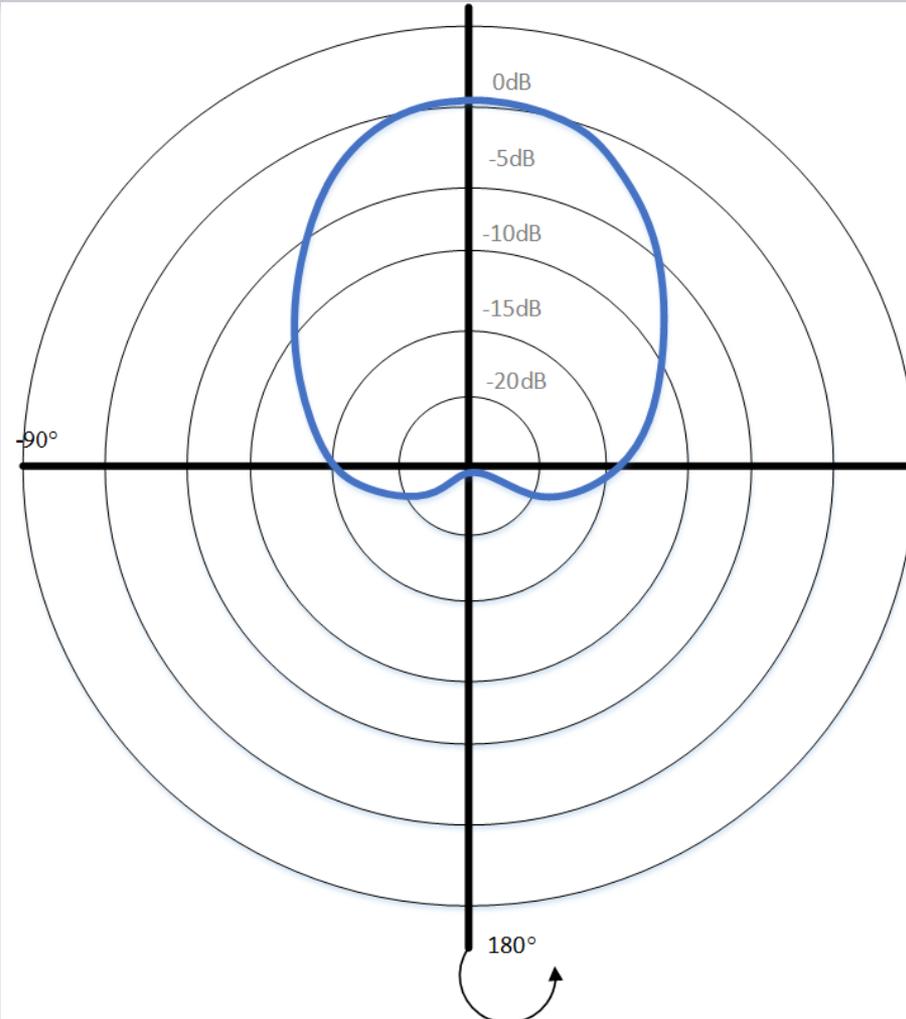


3D Error



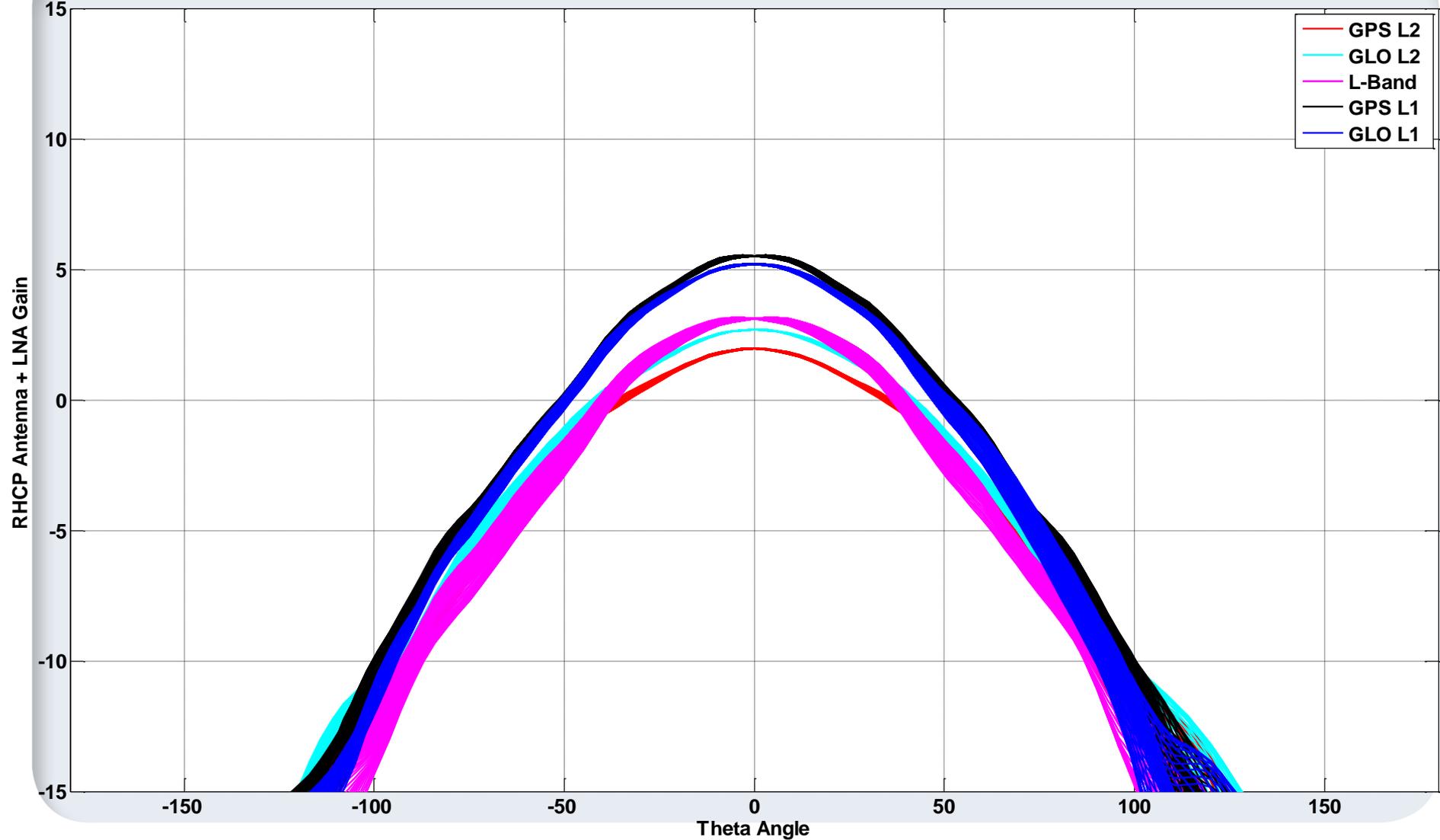
- Troubleshooting eliminate usual suspects
 - Subscription issue?
 - Pigeon sitting on one antenna?

- Root cause:
 - Antenna Performance
 - What does frequency support really mean?



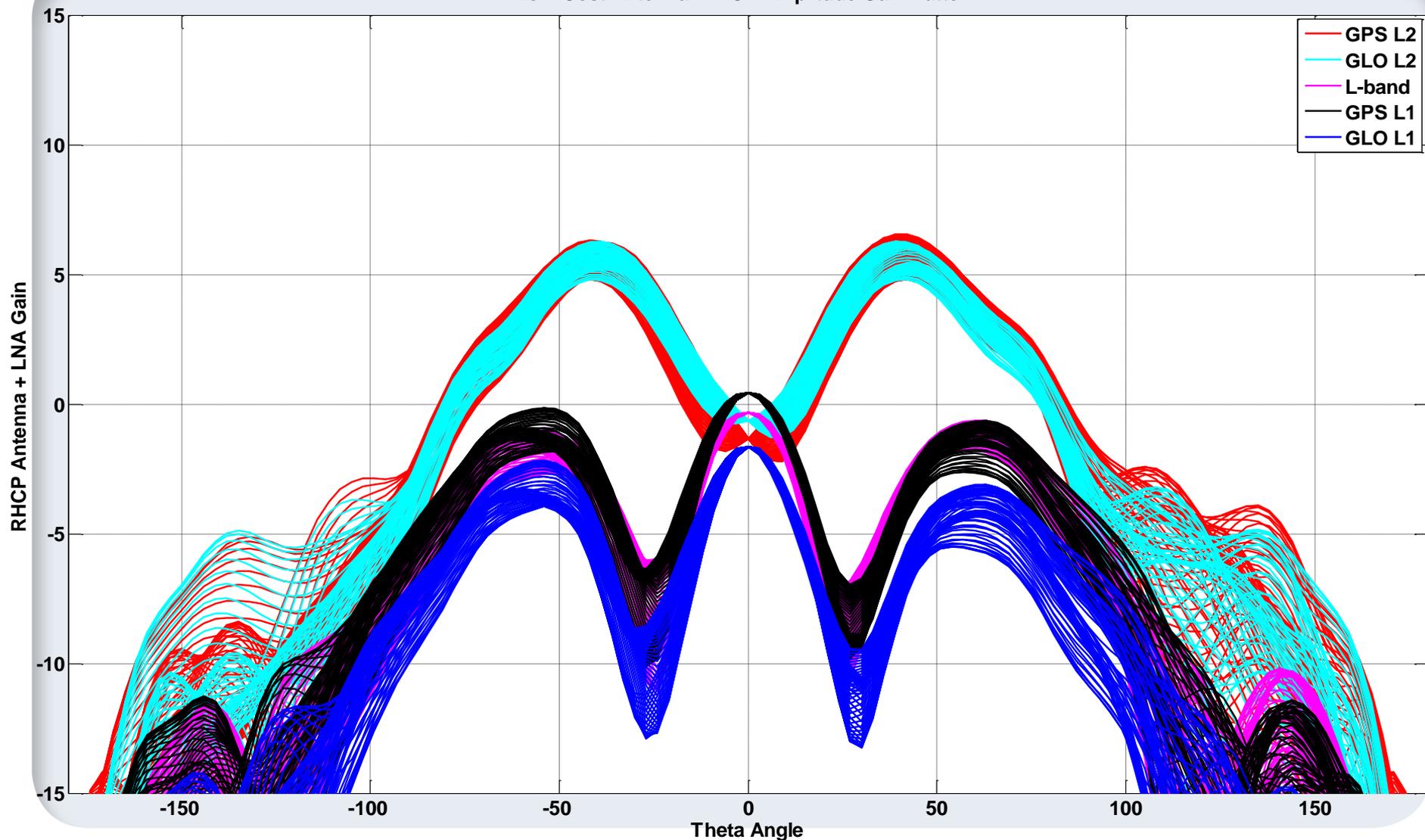
Ideal antenna gain pattern is described by rotating this cross section around the zenith axis

Geodetic Grade Antenna: RHCP Amplitude Gain Pattern



Low Cost Antenna Gain Pattern

Low Cost Antenna: RHCP Amplitude Gain Pattern



- Know your measurement chain!
- Maintain signal quality at each component
- Trade off where you can, but don't sacrifice the fundamentals

- Enjoy your <10cm positioning!

Visit www.insidegnss.com/webinars for:

- PDF of Presentations
- Bibliography

To contact today's panel, email:

info@insidegnss.com

Poll #3

What additional functionality would you like to have in your GNSS? (Select up to two)

- Higher accuracy*
- Greater availability/robustness*
- Greater redundancy*
- Greater integrity*

Ask the Experts – Part 2



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Sara Masterson, P. Eng.

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